

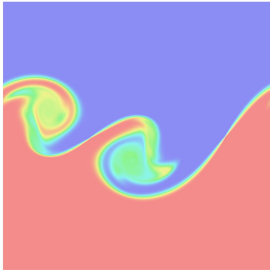
Second order anti-diffusive Lagrange-remap scheme

SIMCAPIAD project

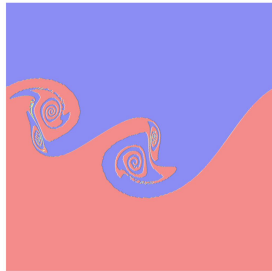
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Samuel KOKH, Frédéric LAGOUTIÈRE & Laurent NAVORET

CEMRACS 2010, Wednesday, August 25 2010

- Numerical simulation of interfaces between two fluids



upwind



anti-diffusive

- **Lagrange-projection** (or Lagrange-remap) schemes
+ **anti-diffusive** tool for the interface
→ **2nd order schemes**

Outline

- ① The model
- ② The numerical scheme
- ③ Second order in space

Outline

- 1 The model
- 2 The numerical scheme
- 3 Second order in space

The 5 - equations model (1)

Sharp interface model between two fluids in one model

$\rho = \rho_1$	$\rho = \rho_0$	density
$u = u_1$	$u = u_0$	velocity
$e = e_1$	$e = e_0$	energy

- compressible Euler system ($u = u_1 = u_0$)

$$\partial_t \rho + \partial_x(\rho u) = 0$$

$$\partial_t(\rho u) + \partial_x(\rho u^2 + p) = 0$$

$$\partial_t(\rho e) + \partial_x[u(\rho e + p)] = 0$$

$$\partial_t(\rho y) + \partial_x(\rho y u) = 0$$

$$\partial_t z + u \partial_x z = 0$$

- $z =$ “color” function **→ “indicator function”**
- $y =$ mass fraction of the phase 1 **→ “conservative variable”**

The 5 - equations model (2)

- $z =$ “color” function

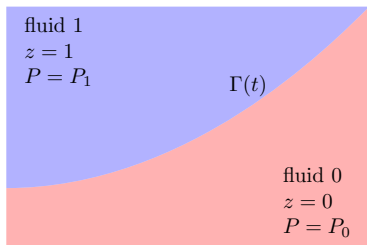
→ “indicator function”

$$\begin{aligned}\rho &= z \rho_1 + (1 - z) \rho_0 && \text{(total density)} \\ \rho u &= z (\rho u)_1 + (1 - z) (\rho u)_0 && \text{(total momentum)} \\ \rho e &= z (\rho e)_1 + (1 - z) (\rho e)_0 && \text{(total energy)}\end{aligned}$$

- pressure

$$\text{in } [z = 1], \quad p = p_1(\rho_1, \varepsilon_1), \quad \varepsilon_1 = e_1 - \frac{u^2}{2}$$

$$\text{in } [z = 0], \quad p = p_0(\rho_0, \varepsilon_0), \quad \varepsilon_0 = e_0 - \frac{u^2}{2}$$



- **theoretically $y = z \in \{0, 1\}$**

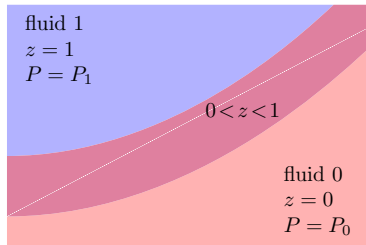
The 5 - equations model (3)

- **numerical diffusion of the interface**
 $y \neq z \in [0, 1]$
- $\rho, \rho u, \rho e, p$ in the region $[0 < z < 1]$

$$\begin{aligned}\rho &= z \rho_1 + (1 - z) \rho_0 \\ \rho u &= z (\rho u)_1 + (1 - z) (\rho u)_0 \\ \rho e &= z (\rho e)_1 + (1 - z) (\rho e)_0\end{aligned}$$

if $0 < z < 1$, $p = p_1(\rho_1, \varepsilon_1) = p_0(\rho_0, \varepsilon_0)$

$$\text{where } \varepsilon_1, \varepsilon_0 \text{ solve } \begin{cases} p_1(\rho_1, \varepsilon_1) = p_0(\rho_0, \varepsilon_0) \\ z \rho_1 \varepsilon_1 + (1 - z) \rho_0 \varepsilon_0 = \rho \varepsilon \end{cases} \quad (\text{isobaric closure})$$



Outline

- ① The model
- ② The numerical scheme
- ③ Second order in space

The numerical scheme

- Lagrange-projection: **separate the acoustic waves / the “material” waves**

$$\partial_t \rho \quad + \quad \partial_x(\rho u) \quad = \quad 0$$

$$\partial_t(\rho u) \quad + \quad \partial_x(\rho u^2 + p) \quad = \quad 0$$

$$\partial_t(\rho e) \quad + \quad \partial_x[u(\rho e + p)] \quad = \quad 0$$

$$\partial_t(\rho y) \quad + \quad \partial_x(\rho y u) \quad = \quad 0$$

$$\partial_t z \quad + \quad u \partial_x z \quad = \quad 0$$

The numerical scheme

- Lagrange-projection: **separate the acoustic waves / the “material” waves**

$$\begin{array}{rclclcl} \partial_t \rho & + & \rho \partial_x u & + & u \partial_x \rho & = & 0 \\ \partial_t(\rho u) & + & \rho u \partial_x u + \partial_x p & + & u \partial_x \rho u & = & 0 \\ \partial_t(\rho e) & + & (\rho e) \partial_x u + \partial_x(pu) & + & u \partial_x(\rho e) & = & 0 \\ \\ \partial_t(\rho y) & + & (\rho y) \partial_x u & + & u \partial_x(\rho y) & = & 0 \\ \partial_t z & + & & + & u \partial_x z & = & 0 \end{array}$$

$\underbrace{\hspace{10em}}_{\text{acoustic}} \qquad \underbrace{\hspace{10em}}_{\text{convection}}$

The numerical scheme

Notation: $\llbracket X \rrbracket_i = (X_{i+1/2} - X_{i-1/2})$

**Lagrange
step**

$(w^n \rightarrow \tilde{w})$

$$L_i \tilde{\rho}_i = \rho_i^n \quad \text{with } L_i = 1 + \frac{\Delta t}{\Delta x} \llbracket u^n \rrbracket_i$$

$$L_i(\tilde{\rho u})_i = (\rho u)_i^n - \frac{\Delta t}{\Delta x} \llbracket \rho^n \rrbracket_i$$

$$L_i(\tilde{\rho e})_i = (\rho e)_i^n - \frac{\Delta t}{\Delta x} \llbracket \rho^n u^n \rrbracket_i$$

**acoustic
scheme**

$$\tilde{y}_i = y_i^n, \quad \tilde{z}_i = z_i^n$$

**Projection
step**

$(\tilde{w} \rightarrow w^{n+1})$

$$\rho_i^{n+1} = \tilde{\rho}_i + \frac{\Delta t}{\Delta x} \llbracket \tilde{\rho} u^n \rrbracket_i - \frac{\Delta t}{\Delta x} \tilde{\rho}_i \llbracket u^n \rrbracket_i$$

$$(\rho u)_i^{n+1} = \tilde{\rho u}_i + \frac{\Delta t}{\Delta x} \llbracket \tilde{\rho u} u^n \rrbracket_i - \frac{\Delta t}{\Delta x} \tilde{\rho u}_i \llbracket u^n \rrbracket_i$$

$$(\rho e)_i^{n+1} = \tilde{\rho e}_i + \frac{\Delta t}{\Delta x} \llbracket \tilde{\rho e} u^n \rrbracket_i - \frac{\Delta t}{\Delta x} \tilde{\rho e}_i \llbracket u^n \rrbracket_i$$

$$(\rho y)_i^{n+1} = \tilde{\rho y}_i + \frac{\Delta t}{\Delta x} \llbracket \tilde{\rho y} u^n \rrbracket_i - \frac{\Delta t}{\Delta x} \tilde{\rho y}_i \llbracket u^n \rrbracket_i$$

convection

$$z_i^{n+1} = \tilde{z}_i + \frac{\Delta t}{\Delta x} \llbracket \tilde{z} u^n \rrbracket_i - \frac{\Delta t}{\Delta x} \tilde{z}_i \llbracket u^n \rrbracket_i$$

The fluxes

Notation: $\llbracket X \rrbracket_i = (X_{i+1/2} - X_{i-1/2})$

Lagrange step

$(w^n \rightarrow \tilde{w})$

**acoustic
scheme**

- Compute $\llbracket u^n \rrbracket, \llbracket p^n \rrbracket$?
→ **Roe type fluxes** for $u_{i+1/2}$ and $p_{i+1/2}$
-

Projection step

$(\tilde{w} \rightarrow w^{n+1})$

convection

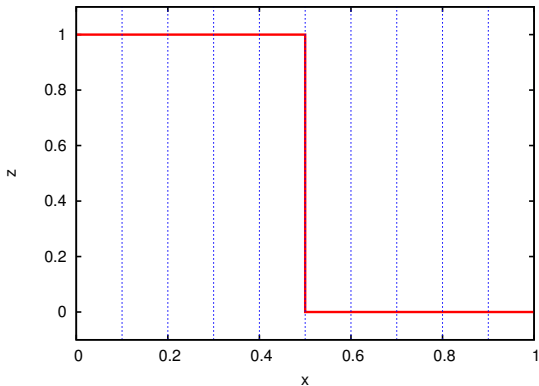
- Compute $\llbracket \tilde{\rho} u^n \rrbracket$?
$$(\tilde{\rho} u^n)_{i+1/2} = \tilde{\rho}_{i+1/2} u_{i+1/2}^n$$
$$\tilde{\rho}_{i+1/2} = z_{i+1/2} (\tilde{\rho}_1)_{i+1/2} + (1 - z_{i+1/2}) (\tilde{\rho}_0)_{i+1/2}$$

→ **upwind flux** for $\tilde{\rho}_1$ and $\tilde{\rho}_0$ computed from y
- Compute $z_{i+1/2}$?
→ **anti-diffusive flux** for z

Anti-diffusive flux

- Anti-diffusive flux** = as downwind as possible
= if $u_{i+1/2} > 0$, $z_{i+1/2}$ is the nearest value to z_{i+1} ensuring stability and consistency

Example: $\partial_t z + u \partial_x z = 0$, with $u = 1$



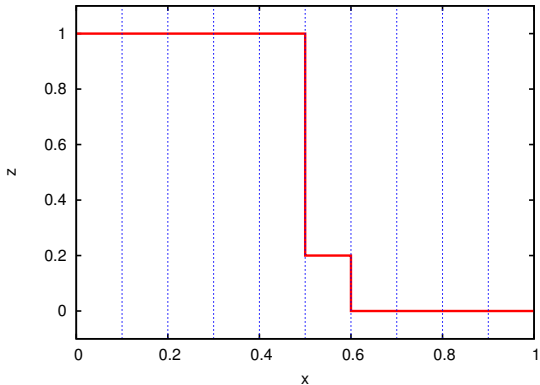
flux at $(x = 0.6)$
= 0

t = 0 Δ t

Anti-diffusive flux

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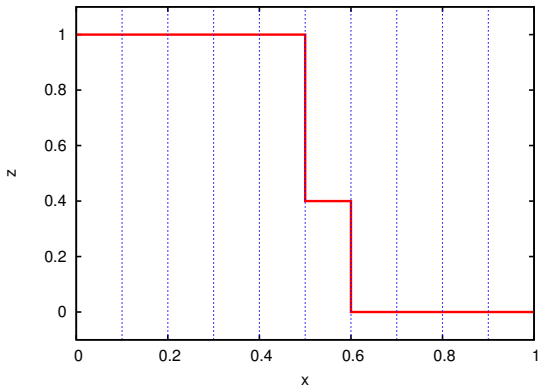
flux at ($x = 0.6$)
= 0

t = 1 Δ t

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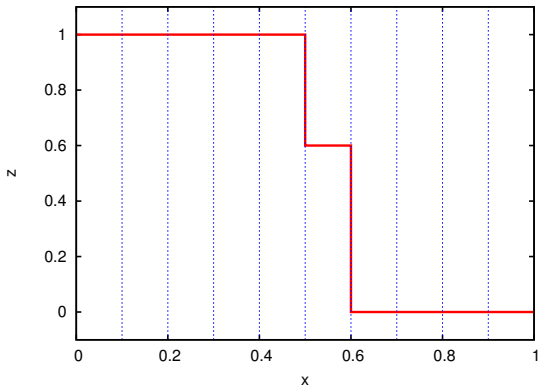
flux at ($x = 0.6$)
= 0

t = 2Δt

Anti-diffusive flux

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ensuring stability and consistency

Example: $\partial_t z + u \partial_x z = 0$, with $u = 1$



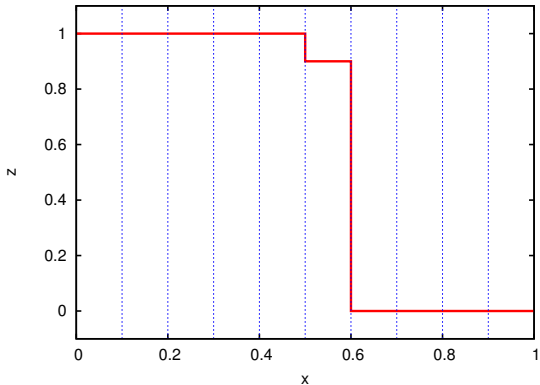
flux at ($x = 0.6$)
= 0

t = 3 Δ t

Anti-diffusive flux

- Anti-diffusive flux** = as downwind as possible
= if $u_{i+1/2} > 0$, $z_{i+1/2}$ is the nearest value to z_{i+1}
ensuring stability and consistency

Example: $\partial_t z + u \partial_x z = 0$, with $u = 1$



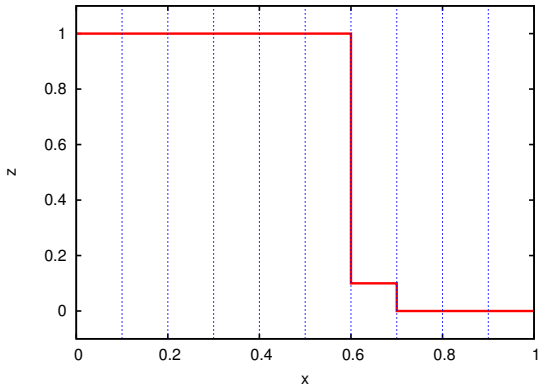
flux at ($x = 0.6$)
= 1

t = 4 Δ t

Anti-diffusive flux

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ensuring stability and consistency

Example: $\partial_t z + u \partial_x z = 0$, with $u = 1$



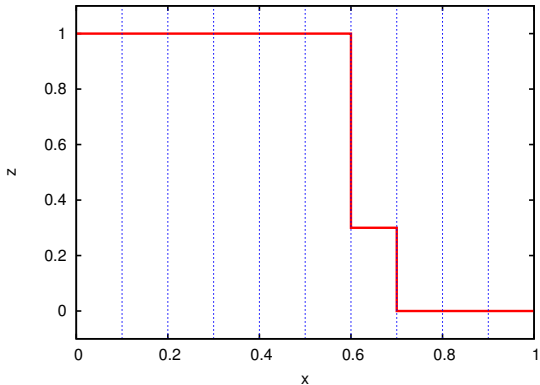
flux at ($x = 0.6$)
= 1

t = 5 Δ t

Anti-diffusive flux

- Anti-diffusive flux** = as downwind as possible
= if $u_{i+1/2} > 0$, $z_{i+1/2}$ is the nearest value to z_{i+1}
ensuring stability and consistency

Example: $\partial_t z + u \partial_x z = 0$, with $u = 1$



flux at ($x = 0.6$)
= 1

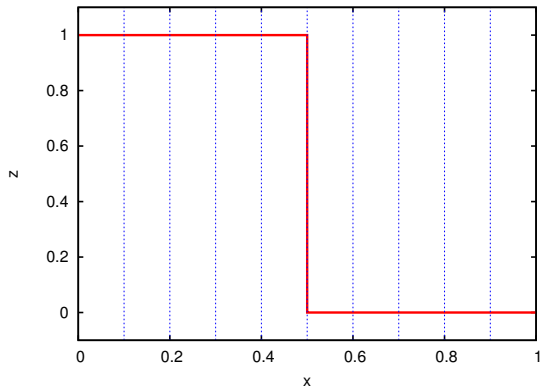
t = 6 Δ t

Upwind flux

Diffusion of the interface with the upwind flux:

$$z_{i+1/2} = \begin{cases} z_i & \text{if } u_{i+1/2} > 0 \\ z_{i+1} & \text{if } u_{i+1/2} < 0 \end{cases}$$

Example: $\partial_t z + u \partial_x z = 0$, with $u = 1$

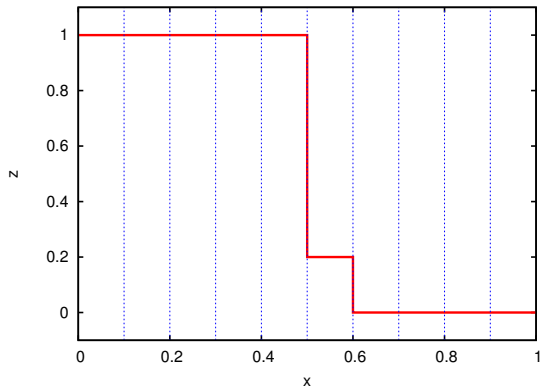


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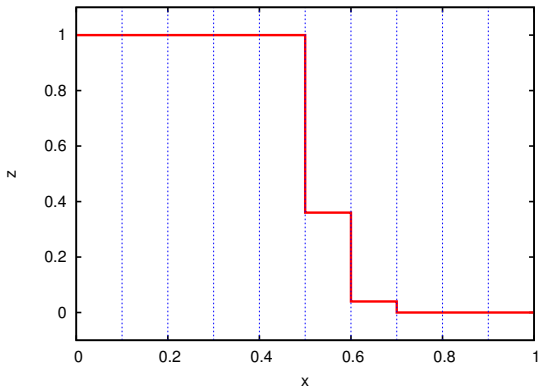
$t = 1\Delta t$

Upwind flux

Diffusion of the interface with the upwind flux:

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Example: $\partial_t z + u \partial_x z = 0$, with $u = 1$



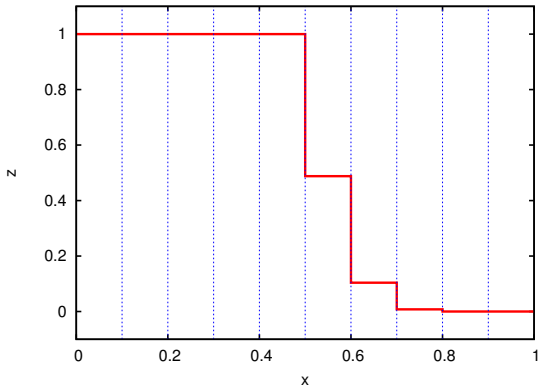
$t = 2\Delta t$

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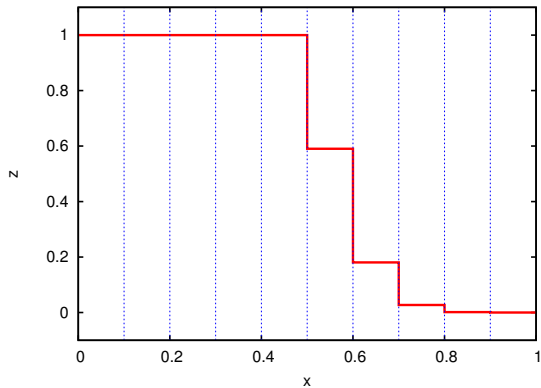
$t = 3\Delta t$

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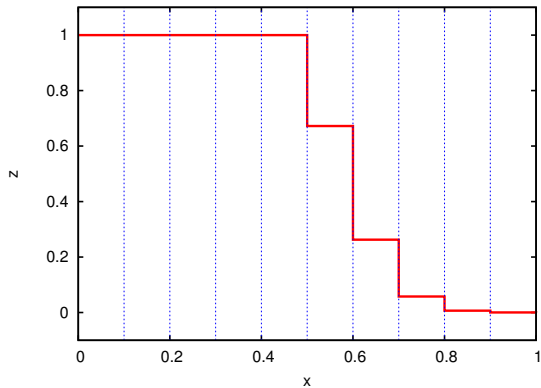
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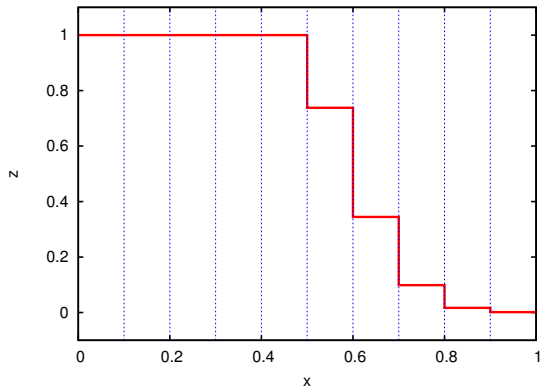


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Example: $\partial_t z + u \partial_x z = 0$, with $u = 1$



$t = 6\Delta t$

Numerical exemple

Sod test-case :

$$\rho_\ell = 1.0$$

$$u_\ell = 0.0$$

$$p_\ell = 1.0$$

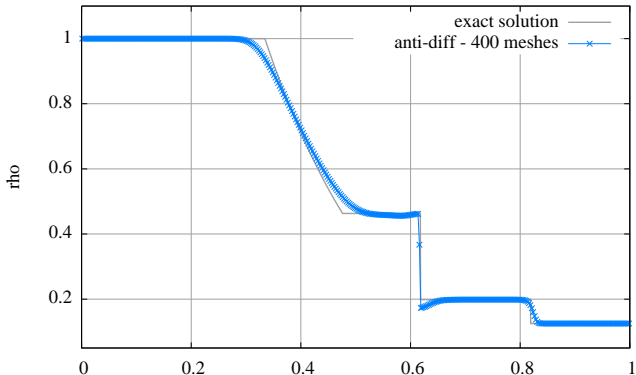
$$z = y = 1$$

$$\rho_r = 0.125$$

$$u_r = 0.0$$

$$p_r = 0.1$$

$$z = y = 0$$



Numerical exemple

Sod test-case :

$$\rho_\ell = 1.0$$

$$u_\ell = 0.0$$

$$p_\ell = 1.0$$

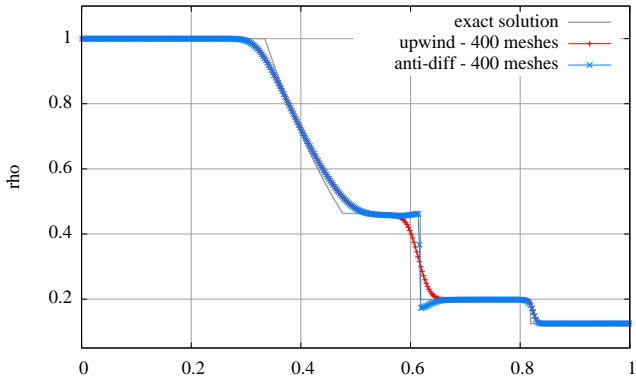
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Outline

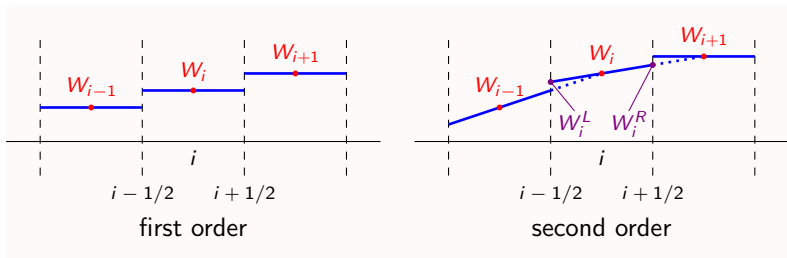
- ① The model
- ② The numerical scheme
- ③ Second order in space

MUSCL strategy

- linear reconstruction for the fluxes

$$\tilde{w}_i(x) = w_i + \sigma_i(x - x_i)$$

$$\sigma_i = \text{minmod} \left(\frac{w_i - w_{i-1}}{\Delta x}, \frac{w_{i+1} - w_i}{\Delta x} \right)$$

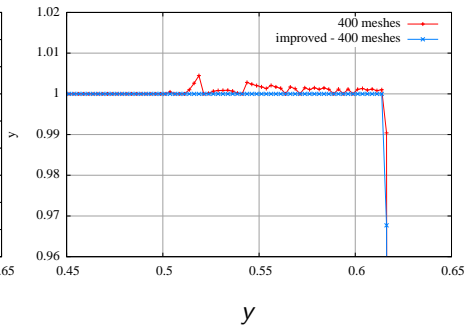
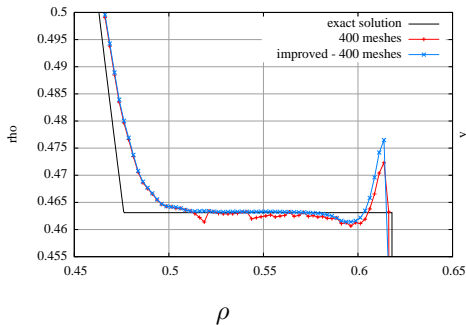


- second order fluxes in the Lagrange step for the Roe fluxes
in the projection step for the upwind fluxes

→ but keep the anti-diffusive flux for z : we can not do better !

Improvement

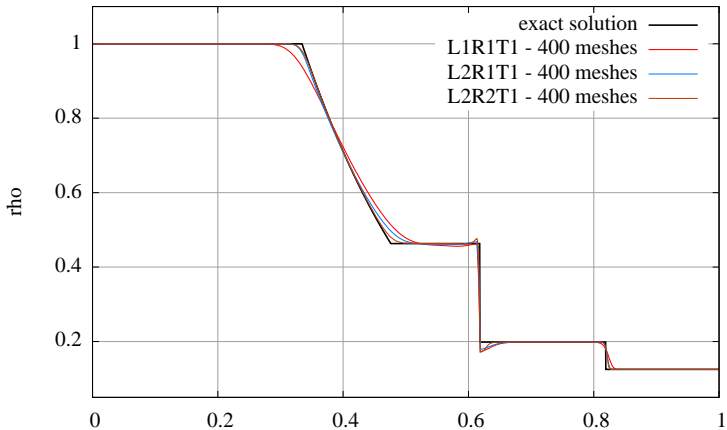
- maximum principle on y is not satisfied (Sod test case)



- in the projection step, keep the **order 1 upwind flux** (i.e. for $(\tilde{\rho}_0)_{i+1/2}, (\tilde{\rho}_1)_{i+1/2}$) in the projection step at the interface $[0 < z < 1]$

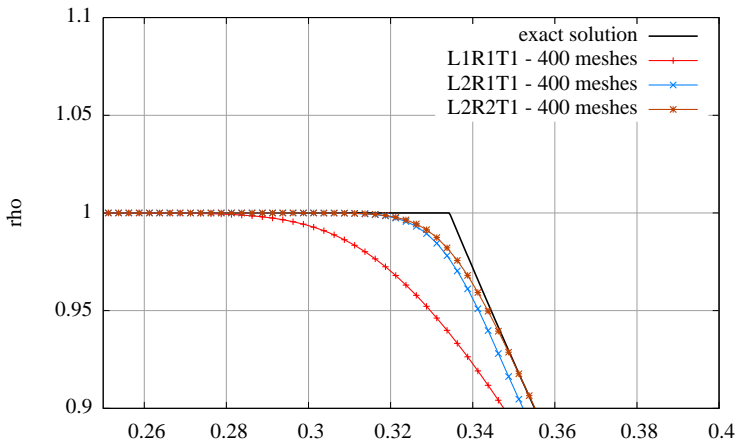
Comparison with order 1

Sod test case



Comparison with order 1

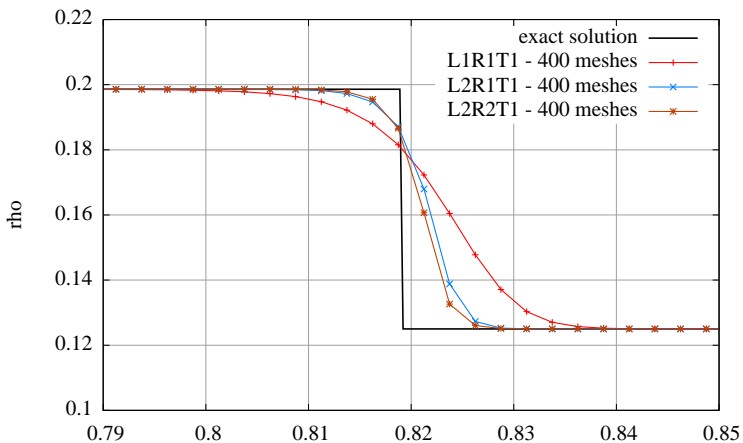
Sod test case: zoom on the rarefaction



the rarefaction is improved

Comparison with order 1

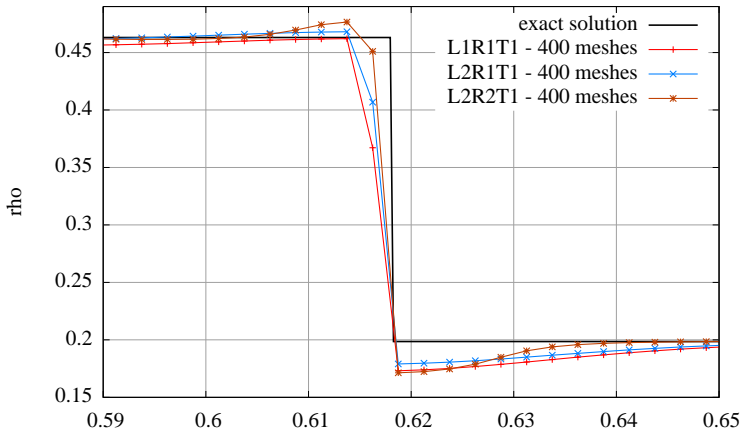
Sod test case: zoom on the shock



the shock is improved

Comparison with order 1

Sod test case: zoom on the contact



the anti-diffusive contact is preserved

Numerical order

Orders for the Sod test-case:

	ρ	u	p
Order 1 upwind	0.63	0.82	0.77
Order 1 anti-diff	0.75	0.82	0.78
Lagrange order 2 anti-diff	0.86	0.88	0.85
Lagrange-projection order 2 upwind	0.83	1.03	1.08
Lagrange-projection order 2 anti-diff	1.08	1.04	1.10

Comments:

- 1 upwind \rightarrow anti-diffusive : improve the order for ρ
- 2 with the order 2 method, orders are improved
but numerical order $\lesssim 1$ (discontinuous solutions)
- 3 Lagrange order 2 + projection of order 2
better than Lagrange order 2

Numerical order

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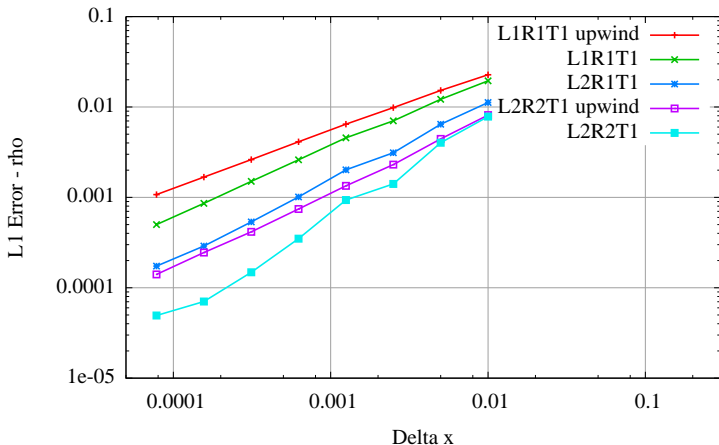
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Numerical order



Comments:

- 1 increasing order + decreasing absolute error
- 2 no possible order 2 (discontinuous solution)

Conclusion

What has been done

- one-dimensional codes (C and Scilab)
- rewriting the Lagrange-projection scheme to integrate Muscl strategy
- deactivation of the Muscl procedure at the interface for preserving the anti-diffusive property

Results

- space order is improved
- no better order in a test case with continuous solution
- wall-heating disappears with mesh refinement

Work in progress

- order 2 in time: no major improvement
- 2D simulations by directionnal splitting
- reducing the wall-heating phenomenon