# Splitting scheme for full and reduced MHD systems. Application to JOREK

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### Outline

Splitting and nonlinear solver: Full MHD

Compatible isogeometric analysis for full MHD

Splitting and nonlinear solver: reduced MHD 199





#### Splitting and nonlinear solver: Full MHD







### Time scheme in JOREK

- Crank-Nicolson or BD2 scheme time scheme.
- Solver: GMRES + Specific Block-Jacobi preconditioning.

#### Advantages/ drawbacks

- Advantages: very efficient in the linear phase. Accurate time scheme.
- Drawbacks: less accurate in the nonlinear phase. Huge memory consumption for Jacobian and PC.

- Idea: splitting + parabolization + Jacobian-free method.
- Drawbacks: Not easy to understand, to modify.
- Aim: time splitting scheme for MHD.







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#### Physic-Based preconditioning

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Figure: Tokamak





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### Model

Resistive MHD model for Tokamak:

 $\begin{cases} \begin{array}{l} \partial_t \rho + \nabla \cdot (\rho \boldsymbol{u}) = \boldsymbol{0}, \\ \rho \partial_t \boldsymbol{u} + \rho \boldsymbol{u} \cdot \nabla \boldsymbol{u} + \nabla p = (\nabla \times \boldsymbol{B}) \times \boldsymbol{B} + \nu \nabla \cdot \boldsymbol{\Pi} \\ \partial_t p + \nabla \cdot (\rho \boldsymbol{u}) + \gamma p \nabla \cdot \boldsymbol{u} = \nabla \cdot ((k_{\parallel} (\boldsymbol{B} \otimes \boldsymbol{B}) + k_{\perp} \boldsymbol{I}_d) \nabla \boldsymbol{T}) + \eta(\boldsymbol{T}) \mid \nabla \times \boldsymbol{B} \mid^2 + \nu \boldsymbol{\Pi} : \nabla \boldsymbol{u} \\ \partial_t \boldsymbol{B} - \nabla \times (\boldsymbol{u} \times \boldsymbol{B}) = \eta(\boldsymbol{T}) \nabla \times (\nabla \times \boldsymbol{B}) \\ \nabla \cdot \boldsymbol{B} = \boldsymbol{0} \end{cases}$ 

- with  $\rho$  the density,  $\boldsymbol{u}$  the velocity ,  $\boldsymbol{p}$  and  $\mathcal{T}$  the pressure and temperature,  $\boldsymbol{B}$  the magnetic field,  $\Pi = \Pi(\nabla \boldsymbol{u}, \boldsymbol{B})$  the stress tensor.
- with  $\nu$  the viscosity,  $k_{\parallel}$ ,  $k_{\perp}$  the thermal conductivities and  $\eta$  the resistivity.

#### Important Properties

Conservation in time:  $\nabla \cdot \boldsymbol{B} = 0$  and

$$\frac{d}{dt}\int \left(\rho\frac{\mid \boldsymbol{u}\mid^2}{2} + \frac{\mid \boldsymbol{B}\mid^2}{2} + \frac{p}{\gamma-1}\right) = 0$$

#### Possible simplification

- $\Box \ \nabla \cdot \boldsymbol{\Pi} \approx \Delta \boldsymbol{u}.$
- Ohmic  $(\eta \mid \nabla \times \boldsymbol{B} \mid^2)$  and viscous heating  $\nu \boldsymbol{\Pi} : \nabla \boldsymbol{u}$  neglected.



# Two stage Energy conserving Splitting

#### Idea

Separate the convection diffusion and magneto-acoustic part. Parabolize the magneto-acoustic part.

Convection - diffusion step:

$$\begin{aligned} &\partial_t \rho + \nabla \cdot (\rho \boldsymbol{u}) = \boldsymbol{0}, \\ &\rho \partial_t \boldsymbol{u} + \rho \boldsymbol{u} \cdot \nabla \boldsymbol{u} = \nu \Delta \boldsymbol{u} \\ &\partial_t \boldsymbol{p} = \nabla \cdot \boldsymbol{q} + \eta(T) \mid \nabla \times \boldsymbol{B} \mid^2 + \nu \boldsymbol{\Pi} : \nabla \boldsymbol{u} \\ &\partial_t \boldsymbol{B} = \eta(T) \nabla \times (\nabla \times \boldsymbol{B}) \end{aligned}$$

Energy balance

$$\partial_t \int \left( \frac{\mid \pmb{B} \mid^2}{2} + \rho \frac{\mid \pmb{u} \mid^2}{2} + \frac{p}{\gamma - 1} \right) = 0$$

Magneto-Acoustic step:

 Splitting and Equilibrium: the balance between pressure gradient and Lorentz force is preserved.



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Energy balance

$$\partial_t \int \left( \frac{\mid \pmb{B} \mid^2}{2} + \rho \frac{\mid \pmb{u} \mid^2}{2} + \frac{p}{\gamma - 1} \right) \leq 0$$

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### Three stage Energy conserving Splitting

Convection - diffusion step:

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Acoustic step:

$$\begin{cases} \partial_t \rho = 0, \\ \rho \partial_t \boldsymbol{u} + \nabla \boldsymbol{p} = 0 \\ \partial_t \boldsymbol{p} + \nabla \cdot (\boldsymbol{p} \boldsymbol{u}) + (\gamma - 1) \boldsymbol{p} \nabla \cdot \boldsymbol{u} = 0 \\ \partial_t \boldsymbol{B} = 0 \\ \nabla \nabla \cdot \boldsymbol{B} = 0 \end{cases}$$

Magnetic step:

$$\begin{aligned} \partial_t \rho &= 0, \\ \rho \partial_t \boldsymbol{u} &= (\nabla \times \boldsymbol{B}) \times \boldsymbol{B} \\ \partial_t p &= 0 \\ \partial_t \boldsymbol{B} &- \nabla \times (\boldsymbol{u} \times \boldsymbol{B}) = 0 \\ \nabla \cdot \boldsymbol{B} &= 0 \end{aligned}$$

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**Splitting and Equilibrium**: the balance is not preserved.



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$$\partial_t \int \left( \frac{|\boldsymbol{B}|^2}{2} + \rho \frac{|\boldsymbol{u}|^2}{2} + \frac{p}{\gamma - 1} \right) = 0$$

**Splitting and Equilibrium**: the balance is not preserved.



### Nonlinear solver for convection-diffusion step

- First possibility: classical Newton method.
- Other possibility: less accurate method but simpler to solve.

#### Idea

Use a specific Picard nonlinear solver which allows to decouple the equation.

We consider a Crank- Nicolson scheme to obtain:

$$\begin{array}{l} \rho^{n+1} + \Delta t \theta \nabla \cdot (\rho^{n+1} \boldsymbol{u}^{n+1}) = R_{\rho}, \\ \rho^{n} \boldsymbol{u}^{n+1} + \Delta t \theta \rho^{n+1} \boldsymbol{u}^{n+1} \cdot \nabla \boldsymbol{u}^{n+1} - \Delta t \theta \nu \Delta \boldsymbol{u}^{n+1} = R_{\boldsymbol{u}} \\ p^{n+1} - \Delta t \theta \nabla \cdot \boldsymbol{q}^{n+1} - \Delta t \theta \eta (T^{n+1}) \mid \nabla \times \boldsymbol{B}^{n+1} \mid^{2} - \Delta t \theta \nu \nabla \boldsymbol{u}^{n+1} : \nabla \boldsymbol{u}^{n+1} = R_{\rho} \\ \boldsymbol{B}^{n+1} - \Delta t \theta \eta (T^{n+1}) \nabla \times (\nabla \times \boldsymbol{B}^{n+1}) = R_{\boldsymbol{B}} \end{array}$$

with 
$$\boldsymbol{q}^{n+1} = (k_{\parallel}(\boldsymbol{B}^{n+1}\otimes \boldsymbol{B}^{n+1}) + k_{\perp}\boldsymbol{I}_d)\nabla T^{n+1}$$





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We write the following picard algorithm:

$$\begin{aligned} & \rho^{k+1} + \Delta t \theta \nabla \cdot (\rho^{k+1} \boldsymbol{u}^{k+1}) = R_{\rho}, \\ & \rho^{n} \boldsymbol{u}^{k+1} + \Delta t \theta \rho^{k} \boldsymbol{u}^{k} \cdot \nabla \boldsymbol{u}^{k+1} - \Delta t \theta \nu \Delta \boldsymbol{u}^{k+1} = R_{\boldsymbol{u}} \\ & p^{k+1} - \Delta t \theta \nabla \cdot \boldsymbol{q}^{k+1} - \Delta t \theta \partial \eta (T^{k}) T^{k+1} \mid \nabla \times \boldsymbol{B}^{k+1} \mid^{2} - \Delta t \theta \nu \nabla \boldsymbol{u}^{k+1} : \nabla \boldsymbol{u}^{k+1} = R_{\rho} \\ & \boldsymbol{B}^{k+1} - \Delta t \theta \eta (T^{k}) \nabla \times (\nabla \times \boldsymbol{B}^{k+1}) = R_{\boldsymbol{B}} \end{aligned}$$

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- Algorithm (at each linear step):
  - □ we solve two independent equations on the magnetic and velocity fields.
  - □ Using  $B^{k+1}$  and  $u^{k+1}$  we compute the two last equations on density and after pressure.



### Nonlinear solver for magneto acoustic step

**First possibility**: classical Newton method. **Problem**: complicate to couple with parabolization.

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$$\begin{cases} \rho^{n+1} = 0, \\ \rho^{n} \boldsymbol{u}^{n+1} + \Delta t \theta \nabla p^{n+1} - \Delta t \theta \left( \nabla \times \boldsymbol{B}^{n+1} \right) \times \boldsymbol{B}^{n+1} = R_{\boldsymbol{u}} \\ p^{n+1} + \Delta t \theta \nabla \cdot \left( p^{n+1} \boldsymbol{u}^{n+1} \right) + \Delta t \theta (\gamma - 1) p^{n+1} \nabla \cdot \boldsymbol{u}^{n+1} = R_{\boldsymbol{p}} \\ \boldsymbol{B}^{n+1} - \Delta t \theta \nabla \times \left( \boldsymbol{u}^{n+1} \times \boldsymbol{B}^{n+1} \right) = R_{\boldsymbol{B}} \end{cases}$$





### Nonlinear solver for magneto acoustic step

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Algorithm (at each linear step):

 $\hfill\square$  We plug the pressure and magnetic field in the velocity equation. We obtain

$$\rho^{n} \boldsymbol{u}^{k+1} - (\Delta t^{2} \boldsymbol{\theta}^{2}) \nabla \left( \nabla \cdot (\boldsymbol{p}^{k} \boldsymbol{u}^{k+1}) + (\gamma - 1) \boldsymbol{p}^{k} \nabla \cdot \boldsymbol{u}^{k+1} \right) + \left( \nabla \times \nabla \times \left( \boldsymbol{u}^{k+1} \times \boldsymbol{B}^{k} \right) \right) \times \boldsymbol{B}^{k} \right]$$

□ We solve this equation and after we compute  $p^{k+1}$  and  $B^{k+1}$  using  $u^{k+1}$  (matrix vector product).



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Compatible isogeometric analysis





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- Isogeometric analysis: use the same basis functions to represent the geometry and physical unknowns.
- **B-Splines**: functions of arbitrary degree p and regularity between  $C^0$  and  $C^{p-1}$ .
- **B-Splines**: by 1D tensor product. Complex geometries obtained by global mapping.
- Compatible space: DeRham sequence







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$$\begin{array}{ccc} \underbrace{curl} & \operatorname{div} \\ H^{1}(\Omega) & \longrightarrow & H(\operatorname{div}, \Omega) & \longrightarrow & L^{2}(\Omega) \\ & & & & \\ & & & & \\ H^{1}(\mathcal{P}) & \longleftarrow & H(\operatorname{div}, \mathcal{P}) & \longleftarrow & L^{2}(\mathcal{P}) \end{array}$$

We can, as in 3D, construct a Discrete DeRham sequence.



- Advantage of Compatible B-Splines space:
  - □ High degree, high regularity.
  - □ Preservation of the properties (3D case here)

$$div_h(Curl_h) = 0$$
,  $Curl_h(grad_h) = 0$ 

and

$$Curl_h^* = Curl_h$$
,  $grad_h^* = div_h$ 

- Dual properties useful for energy conservation, kernel properties for constraints and avoid spurious modes.
- Other point: strong form (equation verified at the coefficient level). Example: Explicit Maxwell.

$$\begin{cases} \boldsymbol{E}^{n+1} = \boldsymbol{E}^n + \Delta t \nabla \times \boldsymbol{B}^n = 0\\ \boldsymbol{B}^{n+1} = \boldsymbol{B}^n - \Delta t \nabla \times \boldsymbol{E}^n = 0\\ \nabla \cdot \boldsymbol{B}^{n+1} = 0, \nabla \cdot \boldsymbol{E}^{n+1} = \rho \end{cases}$$

• We take the **B** equation, choose  $\mathbf{E} \in H(curl)$  and consequently  $\mathbf{B} \in H(div)$ , multiply by test function and integrate to obtain

$$MB_h^{n+1} = MB_h^n + \Delta t CE_h^n$$

with M the mass matrix and C the weak curl matrix.



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Property of the space:  $C = MCurl_h$  therefore we have the following strong form

$$\boldsymbol{B}_{h}^{n+1} = \boldsymbol{B}_{h}^{n} + \Delta t \boldsymbol{C} \boldsymbol{u} \boldsymbol{r} \boldsymbol{I}_{h} \boldsymbol{E}_{h}^{n}$$

• Applying  $div_h$  we obtain  $div_h B_h^{n+1} = 0$ .



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Taking  $B \in H(div)$  we don't have compatibility with the first equation since we have  $\nabla \times B$ . Idea: integrate by part the first equation (weak form)

$$\int (\boldsymbol{E}^{n+1}, \boldsymbol{C}) = \int (\boldsymbol{E}^n, \boldsymbol{C}) + \Delta t \int (\boldsymbol{B}^n, \nabla \times \boldsymbol{C})$$

• Taking  $\boldsymbol{C} \in \boldsymbol{H}(\boldsymbol{curl})$  we obtain a consistent equation.



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At the matrix level, we obtain

$$M_{curl} \boldsymbol{E}^{n+1} = M_{curl} \boldsymbol{E}^n + \Delta t Curl_h^T M_{div} \boldsymbol{B}^n$$

• Taking  $\boldsymbol{C} \in \boldsymbol{H}(\boldsymbol{curl})$  we obtain a consistent equation.



- Additionally we need the commutative projection.
- The 3D projectors are defined by:

$$\widetilde{\Pi}_{h1}^{h} := \left\{ \begin{array}{c} \widetilde{\Pi}_{h1}^{h} f = f_{\rho}^{0} \in V^{h} \\ f_{\rho}^{0}(\mathbf{x}_{k}) = \mathbf{x}_{k}, \quad \forall \mathbf{x}_{k} \in N_{h} \end{array} \right. \quad \widetilde{\Pi}_{L2}^{h} := \left\{ \begin{array}{c} \widetilde{\Pi}_{L2}^{h} \mathbf{f} = f_{\rho}^{3} \in X^{h} \\ \int_{V_{k}} f_{\rho}^{3} = \int_{S_{k}} \mathbf{f}, \quad \forall v_{k} \in \Omega_{h} \end{array} \right.$$

with  $N_h$  the nodes of the mesh.  $\Omega_h$  the cells of the mesh.

$$\widetilde{\Pi}^{h}_{curl} := \begin{cases} \widetilde{\Pi}^{h}_{curl} \mathbf{f} = \mathbf{f}^{1}_{p} \in V^{h}_{curl} \\ \int_{e_{k}} \mathbf{f}^{1}_{p} \cdot \mathbf{t} = \int_{e_{k}} \mathbf{f} \cdot \mathbf{t}, \quad \forall e_{k} \in E_{h} \end{cases} \qquad \widetilde{\Pi}^{h}_{div} := \begin{cases} \widetilde{\Pi}^{h}_{div} \mathbf{f} = \mathbf{f}^{2}_{p} \in V^{h}_{div} \\ \int_{f_{k}} \mathbf{f}^{2}_{p} \cdot \mathbf{n} = \int_{f_{k}} \mathbf{f} \cdot \mathbf{n}, \quad \forall f_{k} \in F_{h} \end{cases}$$

- with  $E_h$  the edges of the mesh.  $\Omega_h$  the faces of the mesh.
- Exemple:  $\rho_2 = \nabla \times (2x(1-x)y(1-y))$ . Comparison between  $L^2$  and commutative projection in H(div):





Numerical example: 2D Maxwell model:

$$\begin{cases} \mathbf{E}^{n+1} = \mathbf{E}^n + \Delta t Curl B^n - \mu_0 \mathbf{J} \\ B^{n+1} = B^n - \Delta trot(\mathbf{E}^n) \\ \nabla \cdot \mathbf{B}^{n+1} = 0, \nabla \cdot \mathbf{E}^{n+1} = \rho \end{cases}$$

- with  $CurlB = \begin{pmatrix} \partial_y B \\ -\partial_x B \end{pmatrix}$  and  $Rot(\boldsymbol{E}) = \partial_x E_y \partial_y E_x$ .
- Property to preserve

$$\nabla \cdot \partial_t \boldsymbol{E} = \partial_t \rho$$
, since  $\partial_t \rho + \nabla \cdot \boldsymbol{J} = 0$ .

Charge conservation for Implicit scheme with 16\*16 cells. Order 3



 Left: Compatible space with commutative projection. Right: Compatible space without commutative projection.



### Three stage Energy conserving Splitting

Magnetic step:

$$\begin{aligned} &\partial_t \rho = \mathbf{0}, \\ &\rho \partial_t \boldsymbol{u} = (\nabla \times \boldsymbol{B}) \times \boldsymbol{B} \\ &\partial_t p = \mathbf{0} \\ &\partial_t \boldsymbol{B} - \nabla \times (\boldsymbol{u} \times \boldsymbol{B}) = \mathbf{0} \\ &\nabla \cdot \boldsymbol{B} = \mathbf{0} \end{aligned}$$

Acoustic step:

$$\begin{array}{l} \partial_t \rho = \mathbf{0}, \\ \rho \partial_t \boldsymbol{u} + \nabla \boldsymbol{p} = \mathbf{0} \\ \partial_t \boldsymbol{p} + \nabla \cdot (\boldsymbol{p} \boldsymbol{u}) + (\gamma - 1) \boldsymbol{p} \nabla \cdot \boldsymbol{u} = \mathbf{0} \\ \partial_t \boldsymbol{B} = \mathbf{0} \\ \nabla \cdot \boldsymbol{B} = \mathbf{0} \end{array}$$

Convection - diffusion step:

$$\begin{cases} \partial_t \rho + \nabla \cdot (\rho \boldsymbol{u}) = 0, \\ \rho \partial_t \boldsymbol{u} + \rho \boldsymbol{u} \cdot \nabla \boldsymbol{u} = 0 \\ \partial_t \rho = 0 \\ \partial_t \boldsymbol{B} = 0 \end{cases}$$

- □ Strong conservation of  $\nabla \cdot \boldsymbol{B} = 0 = = \boldsymbol{B}_h \in \boldsymbol{H}(div)$
- Multiply by v and integrate by part

$$\partial_t \int (\boldsymbol{u}_h, \boldsymbol{v}) + \int (\boldsymbol{B}_h, \nabla \times (\boldsymbol{v} \times \boldsymbol{B}_h)) = 0$$

□ So  $(u_h \times B_h)$ ,  $(ref v) \in H(Curl) ===> u_h \in H(Curl)$ □ Commutative projection needed.

- $\Box \ \boldsymbol{u}_h \in \boldsymbol{H}(\textit{Curl}) = = > \boldsymbol{p} \in \boldsymbol{H}_1$ 
  - Multiply by q and integrate by part

$$\partial_t \int p_h q - \int (p \boldsymbol{u}, \nabla q) - (\gamma - 1)(\boldsymbol{u}, \nabla (p_h q)) = 0$$

Commutative projection needed.

$$\begin{array}{l} \square \ \rho \boldsymbol{u} \in H(Di\boldsymbol{v}) = = = > \rho_h \in L^2. \\ \square \ \text{We that to } \boldsymbol{u} \cdot \nabla \boldsymbol{u} = \nabla \times \boldsymbol{u} \times \boldsymbol{u} + \nabla(\boldsymbol{u}, \boldsymbol{u}) \text{ to obtain} \\ \int \rho(\partial_t \boldsymbol{u}, \boldsymbol{v}) + \int (\nabla \times \boldsymbol{u} \times \boldsymbol{u}, \boldsymbol{v}) - \frac{1}{2} \mid \boldsymbol{u} \mid^2 \nabla \cdot (\rho \boldsymbol{v}) \\ \square \ \text{Energy: strong form of } \rho \text{ equation multiply } \frac{1}{2} \mid \boldsymbol{u}_h \mid^2 \\ \text{ and integrate.} \end{array}$$



### Splitting and nonlinear solver: reduced MHD 199





Inia

### Model

Resistive reduced MHD 1999 model for Tokamak:

$$\begin{array}{l} \partial_t \rho + \boldsymbol{u}_{\perp} \cdot \nabla \rho + \rho \nabla \cdot \boldsymbol{u}_{\perp} = \nabla \cdot (D(\psi) \nabla T) \\ \partial_t T + \boldsymbol{u}_{\perp} \cdot \nabla T + (\gamma - 1) T \nabla \cdot \boldsymbol{u}_{\perp} = \nabla \cdot (\mathcal{K}(\psi) \nabla T) \\ \nabla \times (\hat{\rho} \partial_t \boldsymbol{u}_{\perp}) \cdot \boldsymbol{e}_{\boldsymbol{\phi}} + \nabla \times (\hat{\rho} \boldsymbol{u}_{\perp} \cdot \nabla \boldsymbol{u}_{\perp}) \cdot \boldsymbol{e}_{\boldsymbol{\phi}} + (\nabla R^2 \times \nabla p) \cdot \boldsymbol{e}_{\boldsymbol{\phi}} + \boldsymbol{B} \cdot \nabla j = \nabla \cdot (v \nabla w) \\ \frac{1}{R^2} \partial_t \psi + \boldsymbol{B} \cdot \nabla \boldsymbol{u} = \frac{\eta(T)}{R^2} j \\ j = \Delta^* \psi \\ w = \Delta_{pol} u \end{array}$$

- with *u* the electric potential,  $\psi$  the poloidal magnetic flux, *w* the vorticity and *j* the toroidal current.  $\hat{\rho} = R^2 \rho$ .
- Reduced operators:
  - $\square \quad \boldsymbol{B} = \frac{F_0}{R} \boldsymbol{e}_{\boldsymbol{\phi}} + \frac{1}{R} \nabla \boldsymbol{\psi} \times \boldsymbol{e}_{\boldsymbol{\phi}}$  $\square \quad \boldsymbol{u} = \boldsymbol{u}_{\perp} = -R \nabla \nabla \boldsymbol{u} \times \boldsymbol{e}_{\boldsymbol{\phi}}$

Reduced operators:

$$\square \quad \boldsymbol{B} \cdot \nabla \boldsymbol{I}_d = -\frac{1}{R} [\boldsymbol{\psi}, \boldsymbol{I}_d] + \frac{F_0}{R^2} \partial_{\boldsymbol{\psi}} \boldsymbol{I}_d$$

$$\square \boldsymbol{u}_{\perp} \cdot \nabla = -R[\boldsymbol{I}_d, \boldsymbol{u}]$$

$$\nabla \cdot \boldsymbol{u}_{\perp} = -\frac{1}{R}[R^2, \boldsymbol{u}] = -2\partial_Z \boldsymbol{u}$$

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#### Energy balance

$$\frac{d}{dt}E(t) = \frac{d}{dt}\int \left(\hat{\rho}\frac{|\nabla u|^2}{2} + \frac{|\nabla \psi|^2}{2R^2} + \frac{p}{\gamma-1}\right) \leq \int \eta(T)j^2 + \nu \int w^2$$



# Two stage Energy conserving Splitting

#### Idea

Separate the convection diffusion and magneto-acoustic part. Parabolize the magneto-acoustic part.

Convection - diffusion step:

$$\begin{array}{l} \left\{ \begin{array}{l} \partial_t \rho = \nabla \cdot (D(\psi) \nabla T) \\ \partial_t T = \nabla \cdot (K(\psi) \nabla T) \\ \nabla \times (\hat{\rho} \partial_t \boldsymbol{u}_\perp) \cdot \boldsymbol{e}_{\boldsymbol{\phi}} + \nabla \times (\hat{\rho} \boldsymbol{u}_\perp \cdot \nabla \boldsymbol{u}_\perp) \cdot \boldsymbol{e}_{\boldsymbol{\phi}} = \nabla \cdot (\nu \nabla w) \end{array} \right. \\ \left\{ \begin{array}{l} \frac{1}{R^2} \partial_t \psi = \frac{\eta(T)}{R^2} j \\ j = \Delta^* \psi \\ w = \Delta_{pol} u \end{array} \right. \end{array} \right\}$$
Energy balance

Magneto-Acoustic step:

Splitting: does not preserved the energy balance. Possible to modify the splitting to assure the balance.



### Nonlinear solver for convection-diffusion step

- First possibility: classical Newton method.
- Other possibility: less accurate method but simpler to solve.

#### Idea

Use a specific Picard nonlinear solver which allows to decouple the equation.

We consider a Crank- Nicolson scheme to obtain:

$$\begin{split} \rho^{n+1} &- \theta \Delta t \nabla \cdot (\mathcal{D}(\psi^{n+1}) \nabla \rho^{n+1}) = R_{\rho} \\ \mathcal{T}^{n+1} &- \theta \Delta t \nabla \cdot (\mathcal{K}(\psi^{n+1}) \nabla \mathcal{T}^{n+1}) = R_{\mathcal{T}} \\ \nabla \times (\hat{\rho}^{n} \boldsymbol{u}_{\perp}^{n+1}) \cdot \boldsymbol{e}_{\phi} + \theta \Delta t \nabla \times (\hat{\rho}^{n+1} \boldsymbol{u}_{\perp}^{n+1} \cdot \nabla \boldsymbol{u}_{\perp}^{n+1}) \cdot \boldsymbol{e}_{\phi} - \theta \Delta t \nabla \cdot (\nu \nabla w^{n+1}) = R_{\mu} \\ \frac{1}{R^{2}} \psi^{n+1} - \frac{\eta(\mathcal{T}^{n+1})}{R^{2}} \Delta^{*} \psi^{n+1} = R_{\psi} \\ w^{n+1} &= \Delta_{\rho ol} u^{n+1} \end{split}$$





### Nonlinear solver for convection-diffusion step

- First possibility: classical Newton method.
- Other possibility: less accurate method but simpler to solve.

#### Idea

Use a specific Picard nonlinear solver which allows to decouple the equation.

We write the following picard algorithm:

$$\begin{split} \rho^{k+1} &-\theta \Delta t \nabla \cdot (\mathcal{D}(\psi^{k+1}) \nabla \mathcal{T}^{k+1}) = R_{\rho} \\ \mathcal{T}^{k+1} &-\theta \Delta t \nabla \cdot (\mathcal{K}(\psi^{k+1}) \nabla \mathcal{T}^{k+1}) = R_{\mathcal{T}} \\ \nabla \times (\hat{\rho}^{n} \boldsymbol{u}_{\perp}^{k+1}) \cdot \boldsymbol{e}_{\boldsymbol{\phi}} + \theta \Delta t \nabla \times (\hat{\rho}^{k} \boldsymbol{u}_{\perp}^{k} \cdot \nabla \boldsymbol{u}_{\perp}^{k+1}) \cdot \boldsymbol{e}_{\boldsymbol{\phi}} - \theta \Delta t \nabla \cdot (\nu \nabla \Delta_{pol} \boldsymbol{u}^{k+1}) = R_{u} \\ \frac{1}{R^{2}} \psi^{k+1} - \theta \Delta t \frac{\eta(\mathcal{T}^{k})}{R^{2}} \Delta^{*} \psi^{k+1} = R_{\psi} \end{split}$$

Algorithm (at each linear step):

- □ we solve two independent equations on the poloidal magnetic flux and potential.
- □ Using  $\psi^{k+1}$  and  $u^{k+1}$  we compute the two last equations on density and temperature.



### Nonlinear solver for magneto acoustic step

**First possibility**: classical Newton method. **Problem**: complicate to couple with parabolization.

#### Idea

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Use a specific Picard nonlinear solver which allows to decouple the equation.

We consider a Crank- Nicolson scheme to obtain:

$$\begin{cases} \rho^{n+1} + \theta \Delta t \boldsymbol{u}_{\perp}^{n+1} \cdot \nabla \rho^{n+1} + \theta \Delta t \rho^{n+1} \nabla \cdot \boldsymbol{u}_{\perp n+1} = R_{\rho} \\ T^{n+1} + \theta \Delta t \boldsymbol{u}_{\perp}^{n+1} \cdot \nabla T^{n+1} + \theta \Delta t (\gamma - 1) T^{n+1} \nabla \cdot \boldsymbol{u}_{\perp}^{n+1} = R_{T} \\ \nabla \times (\hat{\rho}^{n} \boldsymbol{u}_{\perp}^{n+1}) \cdot \boldsymbol{e}_{\phi} + \theta \Delta t (\nabla R^{2} \times \nabla p^{n+1}) \cdot \boldsymbol{e}_{\phi} + \boldsymbol{B}^{n+1} \cdot \nabla j^{n+1} = R_{u} \\ \frac{1}{R^{2}} \psi^{n+1} + \theta \Delta t \boldsymbol{B}^{n+1} \cdot \nabla u^{n+1} = R_{\psi} \\ j = \Delta^{*} \psi \end{cases}$$



### Nonlinear solver for magneto acoustic step

First possibility: classical Newton method. Problem: complicate to couple with parabolization.

#### Idea

Use a specific Picard nonlinear solver which allows to decouple the equation.

We write the following picard algorithm:

$$\begin{array}{l} & \int_{-\infty}^{k+1} + \theta \Delta t \boldsymbol{u}_{\perp}^{k+1} \cdot \nabla \rho^{k} + \theta \Delta t \rho^{k} \nabla \cdot \boldsymbol{u}_{\perp}^{k+1} = R_{\rho} \\ & T^{k+1} + \theta \Delta t \boldsymbol{u}_{\perp}^{k+1} \cdot \nabla \rho^{k} + \theta \Delta t (\gamma - 1) T^{k} \nabla \cdot \boldsymbol{u}_{\perp}^{k+1} = R_{T} \\ & \nabla \times (\hat{\rho}^{n} \boldsymbol{u}_{\perp}^{k+1}) \cdot \boldsymbol{e}_{\phi} + \theta \Delta t (\nabla R^{2} \times \nabla \rho^{k+1}) \cdot \boldsymbol{e}_{\phi} + \boldsymbol{B}^{k} \cdot \nabla \Delta^{*} \psi^{k+1} = R_{u} \\ & \frac{1}{R^{2}} \psi^{k+1} + \theta \Delta t \boldsymbol{B}^{k} \cdot \nabla u^{k+1} = R_{\psi} \\ & \zeta \quad j = \Delta^{*} \psi \end{array}$$

- Algorithm (at each linear step):
  - $\hfill\square$  We plug the pressure and poloidal flux equations in the potential equation. We obtain

$$\begin{aligned} \nabla \times (\hat{\rho}^{n} \boldsymbol{u}_{\perp}^{k+1}) \cdot \boldsymbol{e}_{\phi} &- (\Delta t^{2} \theta^{2}) \left[ T^{k} R^{2} \times \nabla \left( \rho^{k} \nabla \cdot \boldsymbol{u}_{\perp}^{k+1} \right) + \rho^{k} R^{2} \times \nabla \left( T^{k} \nabla \cdot \boldsymbol{u}_{\perp}^{k+1} \right) \right. \\ &+ \left( \boldsymbol{B}^{k} \cdot \nabla \left( \Delta^{*} \boldsymbol{B}^{k} \cdot \nabla \boldsymbol{u}^{k+1} \right) \right] \end{aligned}$$

□ We solve this equation and after we compute  $p^{k+1}$  and  $\psi^{k+1}$  using  $u^{k+1}$  (matrix vector product).



#### E.Franck

### Numerical results in JOREK I

- Aim: compare growth rates of the splitting/ full scheme for different  $\Delta t$ .
- Tearing mode. Circular domain. n<sub>Tor</sub> = 3
- Convergence  $\Delta t$  / growth rates

$\Delta t$	Full scheme	
$\Delta t = 3000$	$3.77E^{-4}$	
$\Delta t = 1000$	$3.45E^{-4}$	
$\Delta t = 500$	3.43E <sup>-4</sup>	
$\Delta t = 250$	$3.41E^{-4}$	
$\Delta t = 125$	$3.41E^{-4}$	

$\Delta t$	Splitting scheme
$\Delta t = 1500$	$1.23E^{-4}$
$\Delta t = 1000$	$1.76E^{-4}$
$\Delta t = 500$	$2.64E^{-4}$
$\Delta t = 200$	$3.24E^{-4}$
$\Delta t = 100$	$3.37E^{-4}$

- **Conclusion**: We obtain similar result with a time step 5 times smaller. The splitting under estimate the GR and the full over estimate a little bit.
- **Comment**: test made without picard scheme on the two steps. Picard scheme validate for the convection step not for the magneto-acoustic step.



### Numerical results in JOREK II

- Aim: compare growth rates of the splitting/ full scheme for different  $\Delta t$ .
- Inxflow test case. D-Shape geometry.  $n_{Tor} = 3$
- Convergence  $\Delta t$  / growth rates

$\Delta t$	Full	Spl scheme
1	$6.1E^{-2}$	$4.2 - 5.8E^{-2}, 4.5 - 4.8E^{-2}$
0.5	$6.1E^{-2}$	$4.5 - 5.5E^{-2}, 5.1 - 5.2E^{-2}$
0.25	$6.1E^{-2}$	$5.5 - 5.7E^{-2}, 5.6 - 5.7E^{-2}$
0.125	$6.1E^{-2}$	$6.0 - 6.1E^{-2}, \ 6.05 - 6.1E^{-2}$

- Conclusion: Convergence of the two methods. We obtain similar result with a time step 5 times smaller. For large time step oscillation of the growth rate.
- **Comment**: test made without picard scheme on the two steps.



• Left: Growth rates for the splitting scheme with  $\Delta t = 1$ . Right: Growth rates for the splitting scheme with  $\Delta t = 0.25$ 



### Default of the splitting: resistivity

- **Resistivity**: play an important role in the instability growth-rate.
- Resistivity dependency: the resistivity is given by:

 $\eta(\mathbf{T}) = \eta_0 \mathbf{T}^{-\frac{5}{2}}$ 

Strong nonlinear dependency between resistivity and temperature.

#### main Remark

- □ Main evolution for T: magneto-acoustic step. The evolution of the temperature is important in this step.
- □ **Main problem**: the resistivity term is in the other step. This splitting can explain the error on the growth-rate.
- Better result if resistivity is in the magneto -acoustic step but no compatible with parabolization.

#### Possible solution

- □ Keep a part (constant ?) of the resistivity effect in the magneto acoustic part. Predictor-corrector or other method.
- Iterative splitting. Each step is solver more than one during one time step but simpler step.



### Conclusion

#### Full mhd

- Energy preserving Splitting + compatible space allows:
  - □ Preserve energy at the discrete level in ideal case. More stability ?
  - □ Preserve strongly  $\nabla \cdot \boldsymbol{B} = \boldsymbol{0}$ .
  - $\hfill\square$  In each step we solve simple problems ( elliptic or advection diffusion) + matrix vector product.
  - □ High-order and High-regularity.
  - □ Needs: stabilization for advection and preconditioning for elliptic solvers.

### Splitting for Reduced mhd

- Splitting less efficient as full solver but useful.
- Time step divise by around 5 for a similar accuracy.
- Simpler problems to solve at each step.

#### Following work for reduced MHD

- Picard solver for Magnetic-acoustic step (June).
- Validation of the scheme with Picard solver for each step (July).
- Parabolization for magneto-acoustic step and september (July September).
- Extension to the model 303 and PeTsc for each sub step.

